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Dark Soliton Array for Communication Security

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Abstract

A system of dark soliton array (DSA) for secured optical communication using the multiplexed dark soliton pulses is presented. Different wavelength of input soliton pulses with relevant parameters are fed into the rings system while the radii of the rings are 7 μm , 5 μm and $R_d = 50 \mu\text{m}$. Result shows that the free spectrum range of dark soliton input with the center wavelength of 1503 nm is 0.073 nm. DSA can be obtained using a series of micro ring resonators with input optical solitons of different wavelength, range from $\lambda = 1513 \text{ nm}$ to $\lambda = 1517 \text{ nm}$. The DSA can be tuned and amplified used for many application in optical communication such as security purposes. In transmission link, the long distance link of the multi variable network can be performed using DSA.

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Keywords: Center wavelength, Array generation, Multiplexer, Ring resonator

1. Introduction

In communication application, soliton can be used for long distance optical communication links. For system performance, the required minimum repeater in the link is the key advantage. However the soliton–soliton interaction, soliton collision and dispersion management must be solved [1–2]. To date, several papers have investigated dark soliton behaviors [3–4] where the detection of dark soliton is extremely difficult. Easy way for detect the dark soliton can be obtained using dark-bright conversion system. This means that the dark soliton characteristics can be used as a form of communication security which can be retrieved by the dark–bright soliton conversion [5, 6]. Dark soliton can be converted into a bright soliton after passing through a specific add/drop filter

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[7]. The transmission signals can be transmitted in the form of dark solitons. The specific end user that is connected to the link via the specific add/drop filter can recover the signals. Dark soliton applications have been widely investigated in various applications [8–9]. In this study, the DSA which consists of an array of micro rings will be used for generation of array dark soliton in communication security.

2. Theoretical Simulation

The dark soliton array can be obtained using dark soliton pulses input to a series of micro ring resonator (MRR) in single system. The stationary multiple dark soliton pulses are introduced into the MRR system, as shown in Figure 1. Each input optical field (E_{in}) of the dark soliton pulses input is given by [3].

$$E_{in} = A \tanh \left[\frac{T}{T_0} \right] \exp \left[\left(\frac{z}{2L_D} \right) - i\omega_0 t \right] \quad (1)$$

where A and z are the optical field amplitude and propagation distance, respectively. T is the soliton pulse propagation time in the frame moving at the group velocity, $T = t - \beta_1 z$, where β_1 and β_2 are the coefficient of the linear and the second order terms of Taylor expansion of the propagation constant. $L_D = T_0^2 / |\beta_2|$ is the dispersion length of the soliton pulse. T_0 in the equation is a soliton pulse propagation time at initial input (or collision pulse width), where t is the soliton phase shift time, and the frequency shift of the soliton is ω_0 . Equation (1) describes a pulse that keeps its temporal width invariance as it propagates and, thus, is called a temporal soliton [10]. When a soliton peak intensity ($|\beta_2 / \Gamma T_0^2|$) is given, then T_0 is known. When a soliton pulse is propagated within nonlinear micro ring device, a balance should be achieved between the dispersion length (L_D) and the nonlinear length ($L_{NL} = 1 / \Gamma \phi_{NL}$), where $\Gamma = n_2 k_0$ is the length scale over which dispersive or nonlinear effects make the beam wider or narrower. For a soliton pulse, there is a balance between dispersion and nonlinear lengths, hence, $L_D = L_{NL}$. When light propagates within the nonlinear material (medium), the refractive index (n) of light within the medium is given by

$$n = n_0 + n_2 I = n_0 + \left(\frac{n_2}{A_{eff}} \right) P \quad (2)$$

where n_0 and n_2 are the linear and nonlinear refractive indexes, respectively. I and P are the optical intensity and optical power, respectively. The effective mode core area of the device is given by A_{eff} .

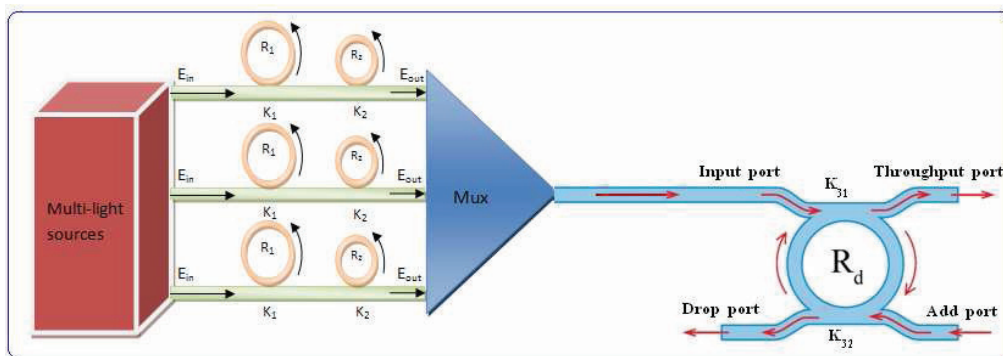


Fig. 1. Schematic of dark soliton array generation. E_{in} , soliton inputs; R , ring radii; κ , coupling coefficients; MUX, optical multiplexer; R_d , add/drop radius; MRR, micro ring resonator.

$$\left| \frac{E_{out}(t)}{E_{in}(t)} \right|^2 = (1-\gamma) \left[1 - \frac{(1-(1-\gamma)x^2)\kappa}{(1-x\sqrt{1-\gamma}\sqrt{1-\kappa})^2 + 4x\sqrt{1-\gamma}\sqrt{1-\kappa}\sin^2(\frac{\phi}{2})} \right] \quad (3)$$

Equation (3) indicates that a ring resonator in this particular case is very similar to a Fabry-Perot cavity, which has an input and output mirror with a field reflectivity, $(1-\kappa)$, and a fully reflecting mirror. κ is the coupling coefficient, and $x = \exp(-\alpha L/2)$ represents a roundtrip loss coefficient, $\phi_0 = kLn_0$ and $\phi_{NL} = kLn_2|E_{in}|^2$ are the linear and nonlinear phase shifts, $k = 2\pi/\lambda$ is the wave propagation number in a vacuum. Where L and α are a waveguide length and linear absorption coefficient, respectively. In this work, the iterative method is used to obtain the results as shown in equation (3), similarly, when the output field is connected and input into the other ring resonators. The optical field of dark soliton pulse is input into a nonlinear series MRR. By using the appropriate parameters, we propose to use the add/drop device. This is given in detail as follows. The optical outputs of a ring resonator add/drop filter can be given by [13].

$$\left| \frac{E_t}{E_{in}} \right|^2 = \frac{(1-\kappa_1) - 2\sqrt{(1-\kappa_1)} \cdot \sqrt{(1-\kappa_2)} e^{-\frac{\alpha}{2}L} \cos(k_n L) + (1-\kappa_2)e^{-\alpha L}}{1 + (1-\kappa_1)(1-\kappa_2)e^{-\alpha L} - 2\sqrt{(1-\kappa_1)} \cdot \sqrt{(1-\kappa_2)} e^{-\frac{\alpha}{2}L} \cos(k_n L)} \quad (4)$$

and

$$\left| \frac{E_d}{E_{in}} \right|^2 = \frac{\kappa_1 \kappa_2 e^{-\frac{\alpha}{2}L}}{1 + (1-\kappa_1)(1-\kappa_2)e^{-\alpha L} - 2\sqrt{(1-\kappa_1)} \cdot \sqrt{(1-\kappa_2)} e^{-\frac{\alpha}{2}L} \cos(k_n L)} \quad (5)$$

where E_t and E_d represents the optical fields of the throughput and drop ports respectively. $\beta = kn_{eff}$ is the propagation constant, n_{eff} is the effective refractive index of the waveguide and the circumference of the ring is $L = 2\pi R$, here R is the radius of the ring. In the following, new parameters will be used for simplification: $\phi = \beta L$ is the phase constant. The chaotic noise cancellation can be managed by using the specific parameters of the add/drop device, which the required signals can be retrieved by the specific users. κ_1 and κ_2 are coupling coefficient of add/drop filters, $k_n = 2\pi/\lambda$ is the wave propagation number for in a vacuum, and where the waveguide (ring resonator) loss is $\alpha = 0.5 \text{ dBmm}^{-1}$. The fractional coupler intensity loss is $\gamma = 0.1$. In the case of add/drop device, the nonlinear refractive index is neglected.

3. Result and Discussion

Generated dark soliton pulse for pulse with 50 ns pulse width and a maximum power of 0.65 W is input into each ring resonator system with different center wavelengths is shown in Figure 1. Suitable ring parameters are used, such as ring radii and ring coupling coefficients, where $R_1 = 7 \text{ }\mu\text{m}$ and $R_2 = 5 \text{ }\mu\text{m}$. To make the system match to the practical device [14], $n_0 = 3.34$ (In-GaAsP/InP).

The effective core areas are $A_{eff} = 0.50 \text{ }\mu\text{m}^2$ and $0.25 \text{ }\mu\text{m}^2$ for MRRs. The waveguide and coupling losses are $\alpha = 0.5 \text{ dBmm}^{-1}$ and $\gamma = 0.1$, respectively, and the coupling coefficients κ of the MRRs range from 0.03 to 0.1. The nonlinear refractive index is $n_2 = 2.2 \times 10^{-13} \text{ m}^2/\text{W}$. In this case, the waveguide loss used is $\alpha = 0.5 \text{ dBmm}^{-1}$. However, more parameters are used, as shown in Figure 1.

The input dark soliton pulse is chopped (sliced) into the smaller signals R_1 and R_2 , and the filtering signals within add/drop ring R_d are seen. We find that the output signal from R_2 is larger than that from R_1 due to the different core effective areas of the rings in the system. However, the effective areas can be transferred from $0.50 \text{ }\mu\text{m}^2$ and $0.25 \text{ }\mu\text{m}^2$ with some losses. The soliton signals in R_d enter the add/drop filter, where the dark soliton conversion can be performed by using Equation (4) and (5). Here, a different dark soliton wavelength is input into the MRR system and

the parameters of the system are set as the same. For instance, the dark solitons are input into the system at the center wavelengths $\lambda_1 = 1501$ nm, $\lambda_2 = 1503$ nm, and $\lambda_3 = 1505$ nm.

When a dark soliton propagates into the MRR system, the dark soliton collision (modulation) in the MUX system and the filtering signals within the add/drop ring (R_d) occur as shown in Figure 1. The dark soliton is generated by multilight sources at the center wavelength $\lambda_1 = 1503$ nm and the filtering signals are as shown in Figure 2. The free spectral range (FSR) and the amplified power of 2.15 nm and 80W of the dark soliton are obtained when, in this case, the spectral width or called it full width at half-maximum (FWHM) of 0.073 nm is achieved. Different center wavelength are input to the micro rings system and filtered by the second ring resonator in each line of the proposed system as shown in Figure 3. The multiplexed output signals from the system is shown in Figure 3(g)

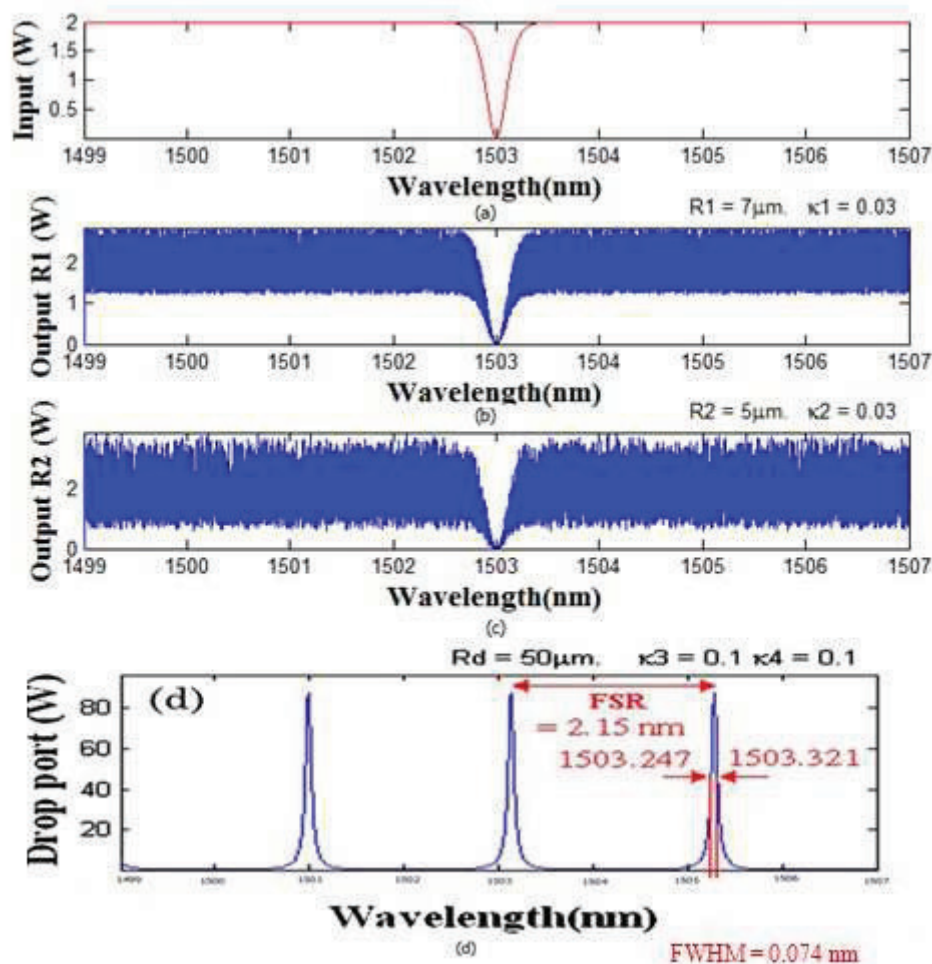


Fig. 2: Simulation result of the dark solitons within the series MRRs when the dark soliton input wavelength is 1503 nm: (a) dark soliton input, (b) and (c) dark solitons in rings R_1 and R_2 , and (d) the drop port signals

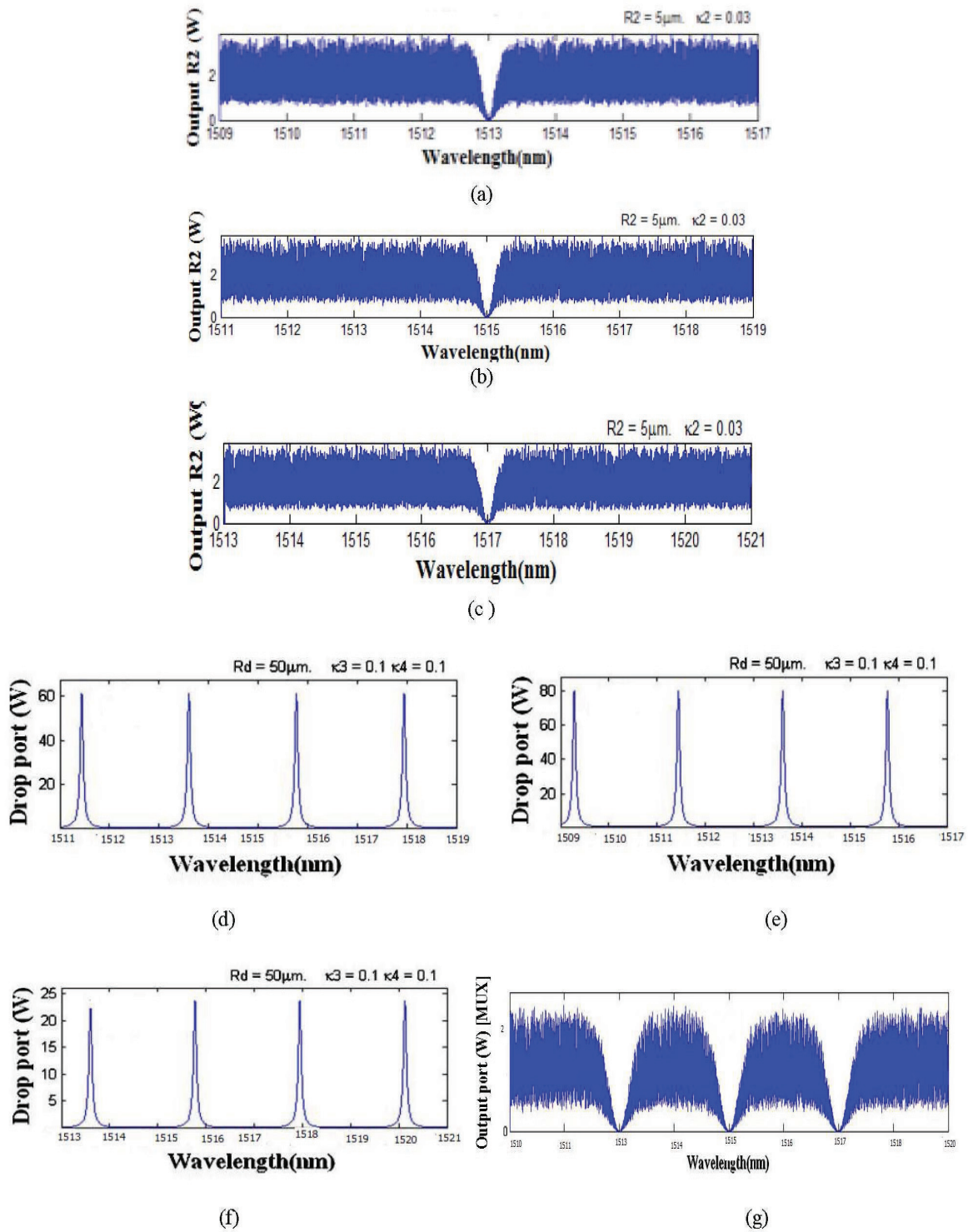


Fig. 3: Simulation result of the dark soliton array when the dark soliton input wavelengths are 1513 nm, 1515 nm, and 1517 nm: (a), (b), and (c) are the output signals R_2 , and (d), (e), and (f) are the drop port signals; (g) dark soliton array

In Figure 3, the dark soliton array generated by multilight sources at center wavelengths of $\lambda_1 = 1513$ nm, $\lambda_2 = 1515$ nm, and $\lambda_3 = 1517$ nm is presented.

3. Conclusion

We have presented the use of ring resonators to generate dark soliton arrays in which the multiplexed dark soliton pulses can be seen by using a light pulse in fiber optic loop or MRR systems. First, the multiple dark solitons are input into the series MRRs, through which multiplexed dark solitons with different center wavelengths, i.e., dark soliton arrays, can be obtained. In this study, dark soliton with FSR and amplified power respectively of 2.15 nm and 80 W can be obtained at the center wavelength of 1503 nm.

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